

Thermal Simulation Report of Bonded Fin Heat Sink





Custom Thermal Solutions - Quick Ramp Manufacturing - Lowest Landed Cost

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- Specification
- Thermal Analysis Condition
- Simulation Results
- Optimization
- Conclusion



Fundamental Specification

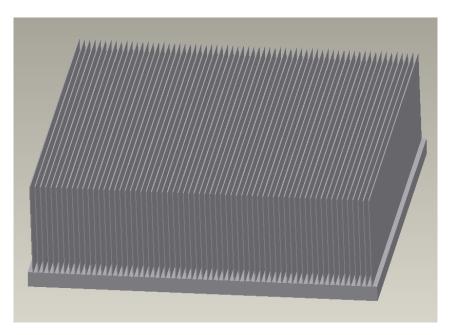
- ❖ Ambient temperture: 35 °C
- ♦ Devices: 2 IGBTs

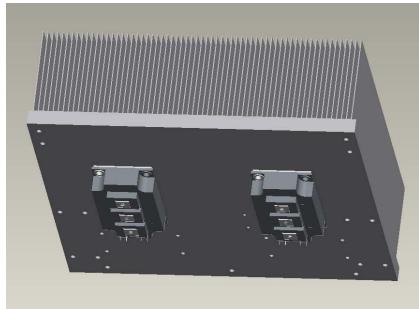
 Total Power = 1500W, 1750W, 2000W
- ❖ Air flow: Provided by two Suntronix SJ1751HA2 (172 x 150 x 57mm)
 - ♦ Maximum air flow = 240CFM (at 3400RPM)
 - **♦** Maximum static pressure = 0.72inH₂O (at 3400RPM)
- * Heat sink material:
 - **❖**Base: Al6063T5
 - **❖**Fin: Al1100



Fundamental Specification

System layout

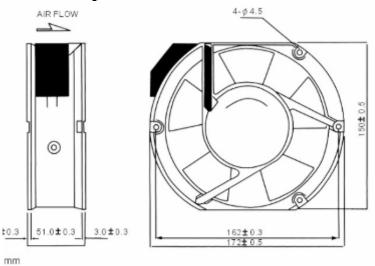


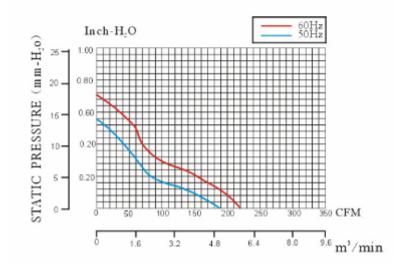




Fundamental Specification

Fan specification







| Model | Part Number Terminal LeadWre | Bearing System | Rated Voltage | Freq. | Current | Input Power | Speed | Flow | Static Pressure | Noise Level | Weigh |
|-----------|------------------------------------|-------------------|------------------|-------|-----------|----------------|-----------|---------|--------------------|----------------|-------|
| | | | (V) | (Hz) | (A) | (W) | (RPM) | (CFM) | (Inchille) | (dB-A) | (g) |
| (型號) | (執予/出建) | (培林) | (電景) | (與車) | (電流) | (功率) | (株法) | (風景) | (89.00) | (株音慎) | (支援 |
| SJ1751HA1 | 1751HA1BAT(L) | Ball | 110/120 | 50/60 | 0.20/0.25 | 22/30 | 2850/3400 | 210/240 | 0.57/0.72 | 50/57 | 920 |
| 5J1751HA2 | 1751HA2BAT(L) | Ball | 220/240 | 50/60 | 0.10/0.13 | 22/30 | 2850/3400 | 210/240 | 0.57/0.72 | 50/57 | 920 |



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Thermal Analysis Condition

❖ Flow model: Turbulent (zero-equation)

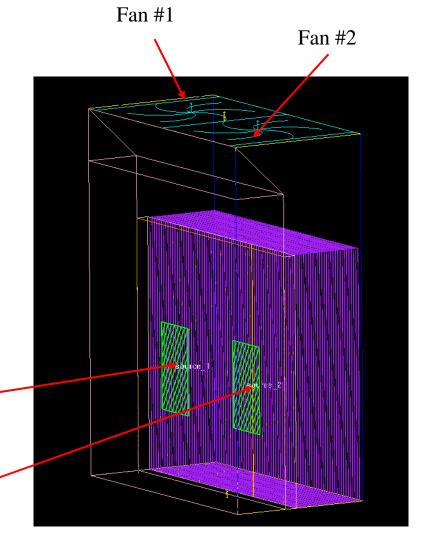
* Flow regime: forced convection

❖ Ambient temperture: 35 °C

***** Devices:

Source-1 = 750W, 875W, 1000W

Source-2 = 750W, 875W, 1000W



Source #1

Source #2

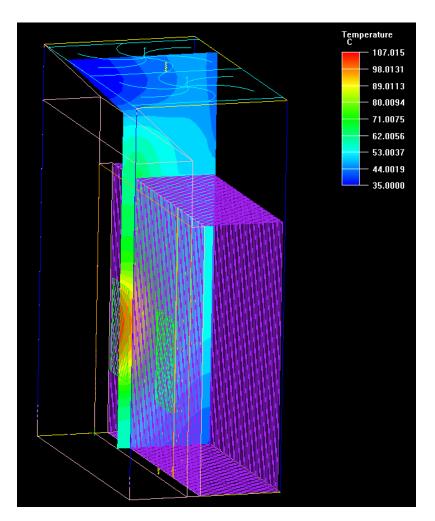


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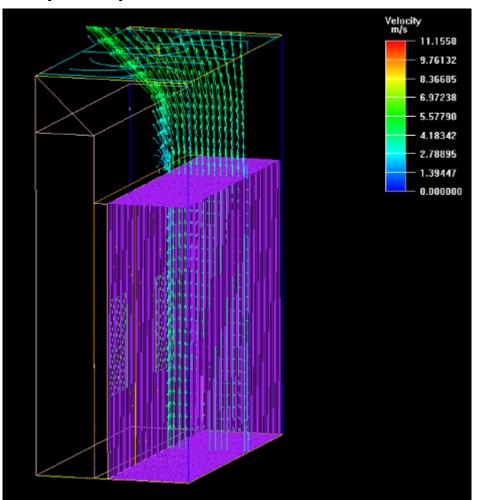


❖ Temperature Distribution (Z-dir.)



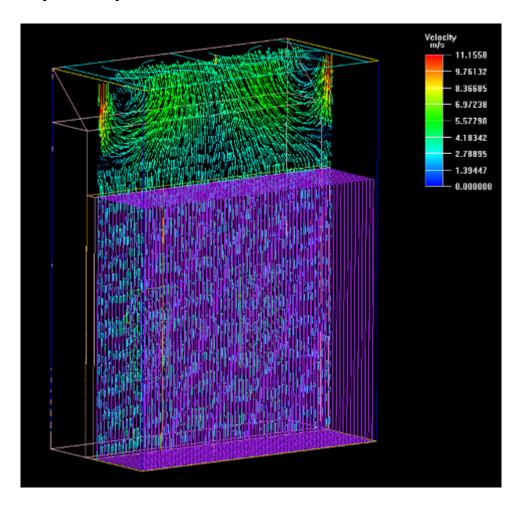


Velocity Profile (Z-dir.)



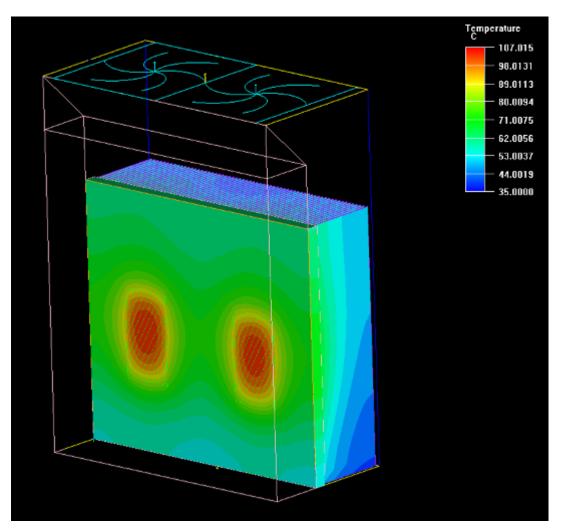


Velocity Profile (X-dir.)





❖ Temperature Distribution on Heat Sink Surface





❖ Summary

| Model | Source-1 | Source-2 | Source-1 | Source-2 | Source-1 | Source-2 |
|------------|----------|----------|----------|----------|----------|----------|
| Power (W) | 750 | 750 | 875 | 875 | 1000 | 1000 |
| Tcase (°C) | 88.87 | 88.24 | 97.61 | 97.13 | 107.2 | 107.3 |
| Tamb (°C) | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |



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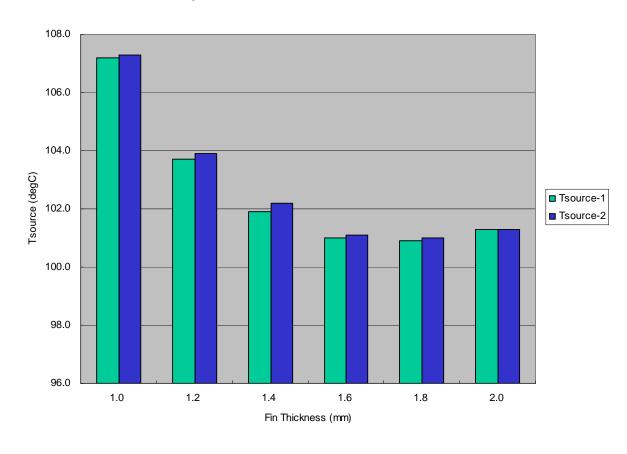
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Optimization

❖ Temperature variation with increased thickness (Power=1000W+1000W, Fin number=64)

| Fin Thickness (mm) | Tsource-1 (°ℂ) | Tsource-2 (°ℂ) |
|--------------------------|-------------------|-------------------|
| 1.0 | 107.2 | 107.3 |
| 1.2 | 103.7 | 103.9 |
| 1.4 | 101.9 | 102.2 |
| 1.6 | 101.0 | 101.1 |
| 1.8 | 100.9 | 101.0 |
| 2.0 | 101.3 | 101.3 |

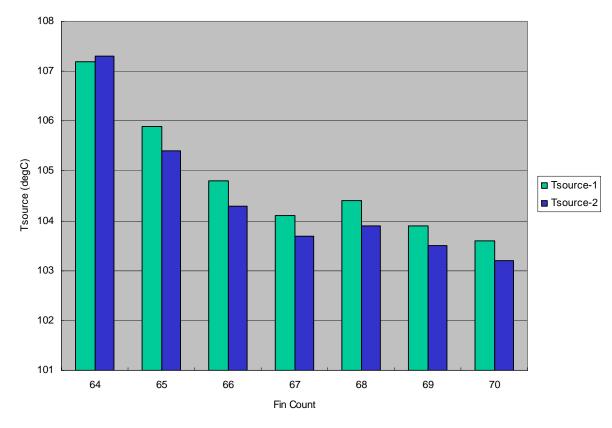




Optimization

❖ Temperature variation with increased fin count (Power=1000W+1000W, Fin thickness=1.0mm)

| Fin Count | Tsource-1 (°ℂ) | Tsource-2 (°C) |
|-----------|-------------------|-------------------|
| 64 | 107.2 | 107.3 |
| 65 | 105.9 | 105.4 |
| 66 | 104.8 | 104.3 |
| 67 | 104.1 | 103.7 |
| 68 | 104.4 | 103.9 |
| 69 | 103.9 | 103.5 |
| 70 | 103.6 | 103.2 |





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Based on the simulation results, the thermal performance of current design can be improved by increasing the fin thickness from 1.0mm to 1.6mm. On the other hand, a minor improvement is also observed when the fin count is increased from the original 64 to 67.



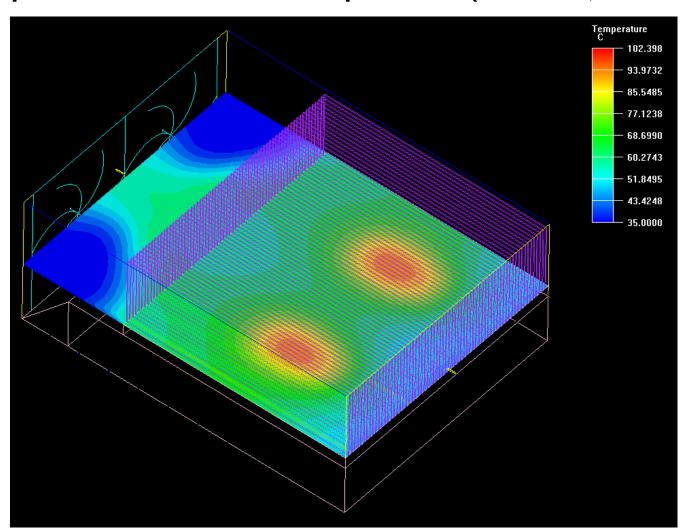
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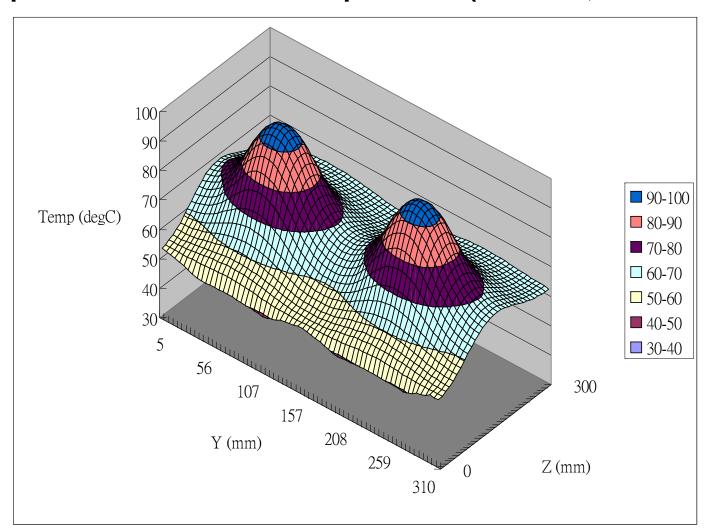
Appendix

❖ Temperature Distribution on a plane cut (X=15mm, Fin bottom)



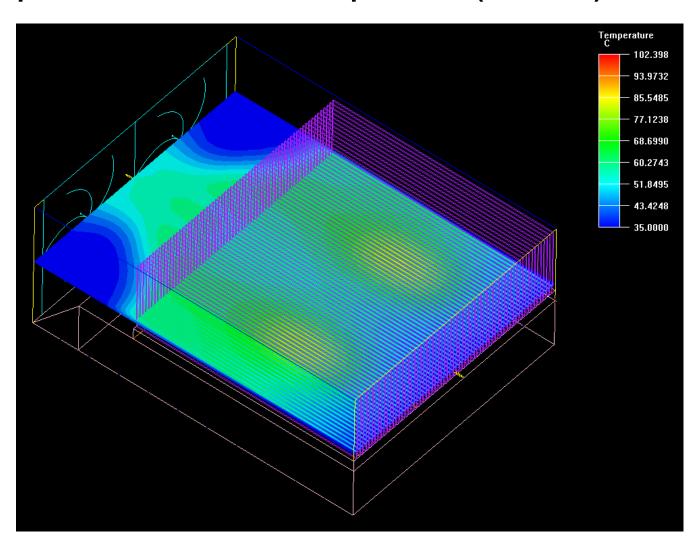


❖ Temperature Distribution on a plane cut (X=15mm, Fin bottom)



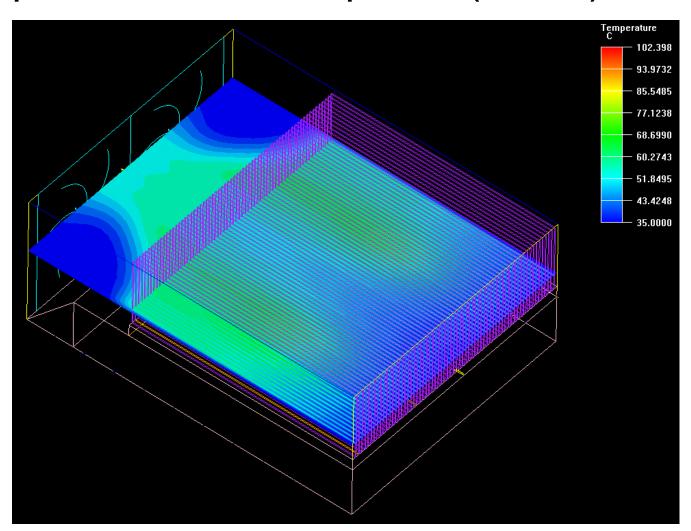


❖ Temperature Distribution on a plane cut (X=25mm)





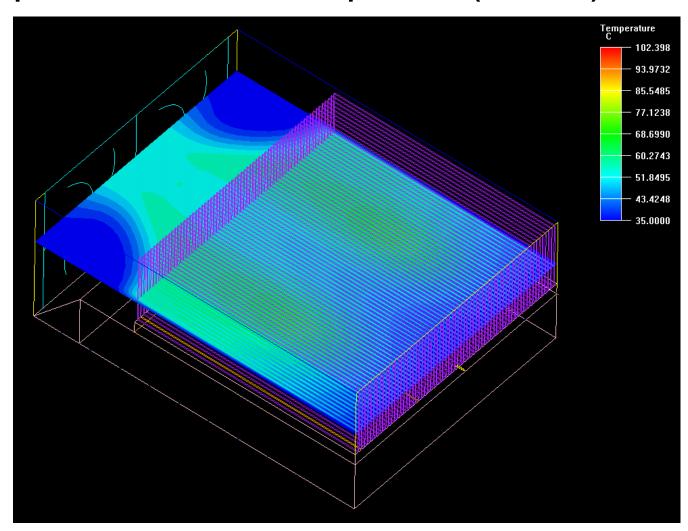
❖ Temperature Distribution on a plane cut (X=35mm)





Appendix

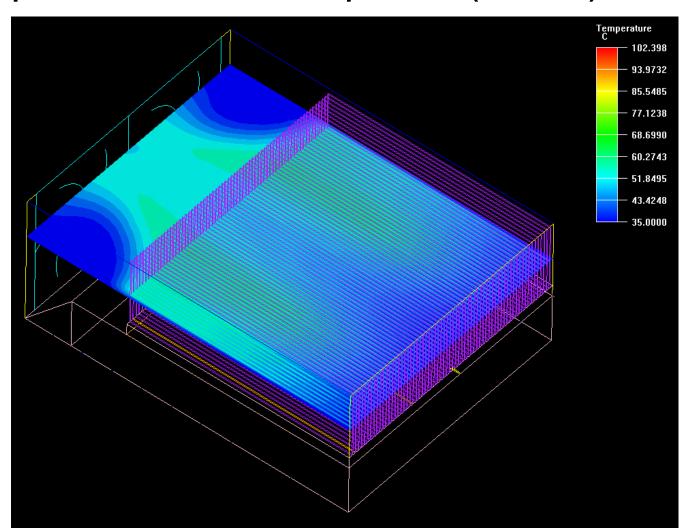
❖ Temperature Distribution on a plane cut (X=45mm)





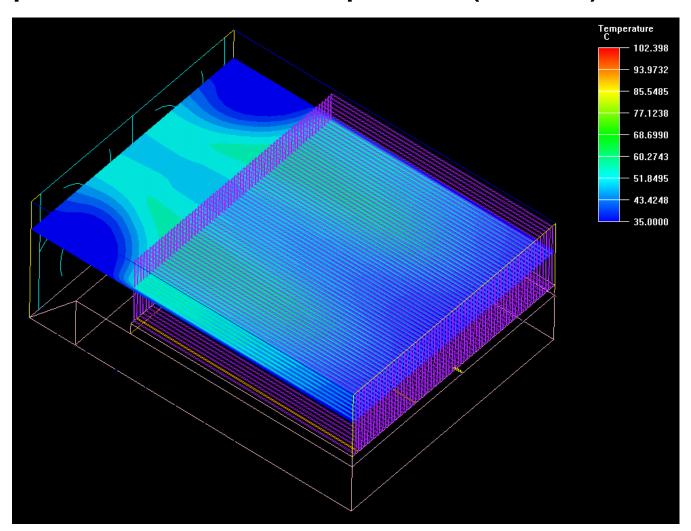
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❖ Temperature Distribution on a plane cut (X=55mm)



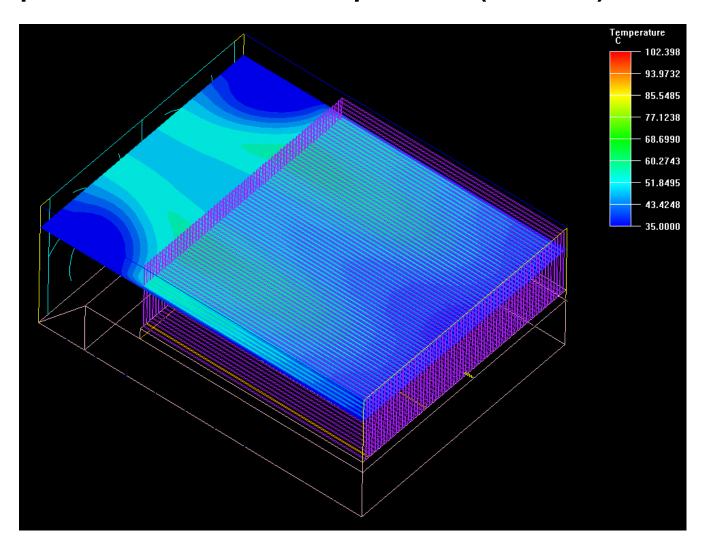


❖ Temperature Distribution on a plane cut (X=65mm)



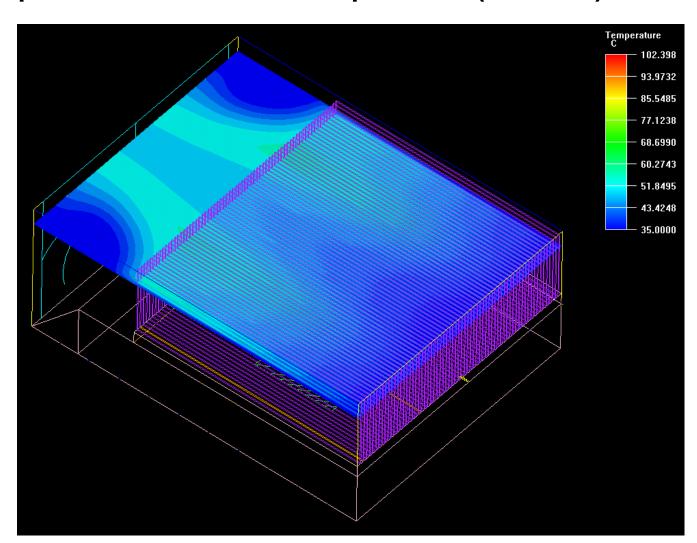


❖ Temperature Distribution on a plane cut (X=75mm)



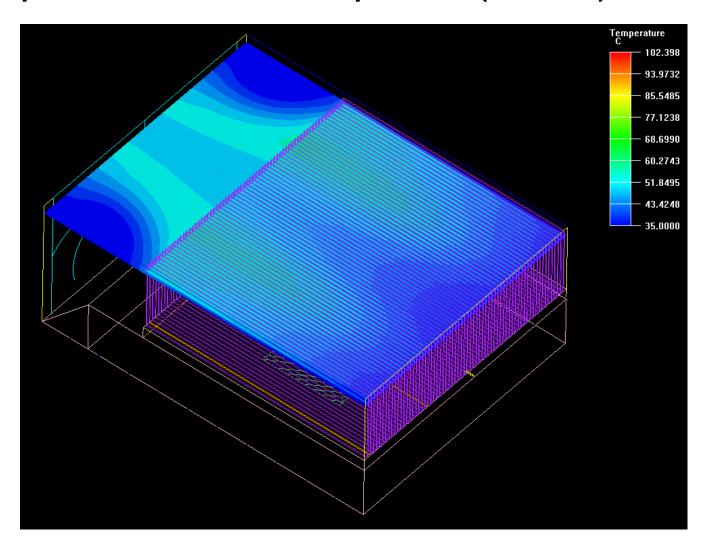


❖ Temperature Distribution on a plane cut (X=85mm)



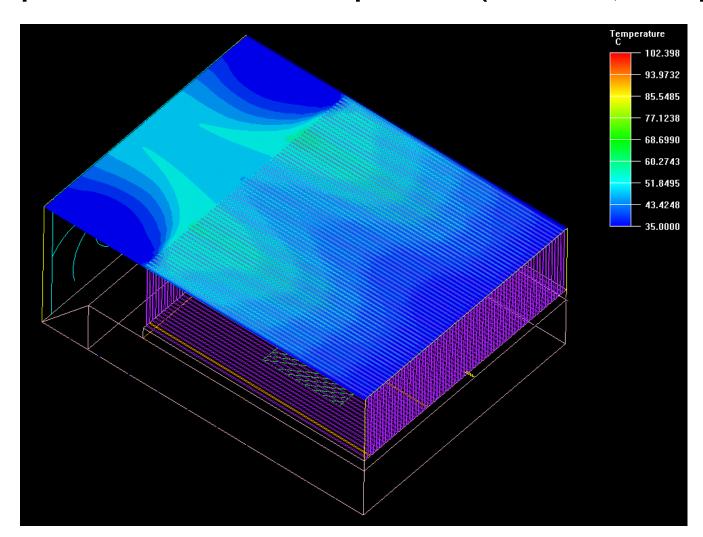


❖ Temperature Distribution on a plane cut (X=95mm)



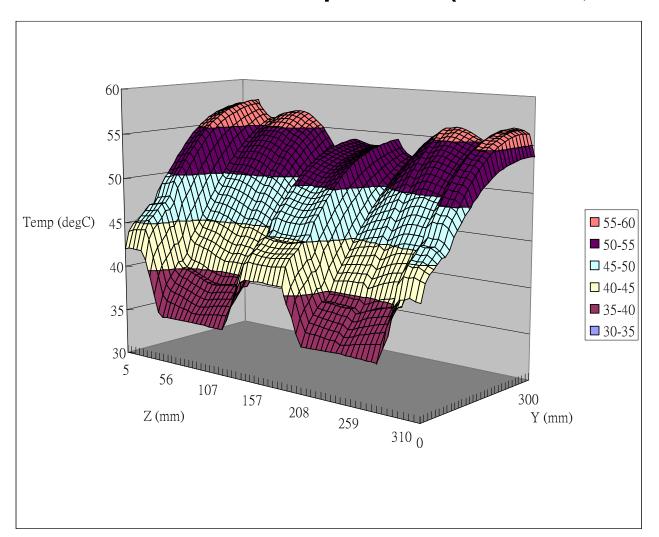


❖ Temperature Distribution on a plane cut (X=105mm, Fin Tip)





❖ Temperature Distribution on a plane cut (X=105mm, Fin Tip)





Appendix (Discussion on fin effective height)

The temperature indeed decreases from the bottom to the tip of the fins. As can be observed from the 3D graph on P. 21, the heat sources generate two peaks on the temperature profile of the plane at X=15mm which is located at the bottom of the fins. From P. 21 to P. 30, the temperature gradually decreases toward to ambient temperature 35° C. The temperature profile of the plane at X=105mm does not show any peaks because the temperature is averaged by the lower temperature ambient flow.

By definition, the fin does not have any effect for heat transfer if the surface temperature is almost the same as the ambient temperature. Therefore, the fin is only effective only for a certain height, any height above the effective height is not helpful to the heat transfer but will increase the flow resistance.

To evaluate if the fin is over the effective height, we can simply judge from the 3D graph on P. 31. Though the temperature at the inlet (Y=0mm) is only slightly above ambient temperature 35 $^{\circ}$ C, the temperature increases quickly as the heat conducted through the fins are absorbed by the flow passed by. At the outlet (Y=300mm), the fin tip temperature can be even as high as over 55 $^{\circ}$ C. Therefore, we can conclude that the fins in this design is still under the effective height and all the fin area is effective for the heat convection.